## Plasticity correction

- Metals will yield when $\sigma=\sigma_{0}$ and a plastic zone will exist at the crack tip.
- Up to $r=r_{p}, \sigma_{y}>\sigma_{o}, r_{p}=$ plastic zone size
- Consider the stresses existing directly ahead of the crack where $\theta=0$
$\begin{aligned} & \text { At elastic-plastic } \\ & \text { boundary }\end{aligned} \sigma_{y}=\frac{K}{\sqrt{2 \pi r_{p}}}=\sigma_{o}$

$$
r_{p}=\frac{K^{2}}{2 \pi \sigma_{o}^{2}}=\frac{\sigma^{2} a}{2 \sigma_{o}^{2}}
$$



## Irwin's correction

- Irwin proposed that the existence of a plastic zone makes the crack act as if it were longer than its physical size.
- As a result of crack-tip plasticity the displacements are larger and the stiffness is lower than for elastic situation.
- The effective crack length is the actual length plus the radius of the plastic zone.

$$
a^{\prime}=a+r_{p}
$$

$$
r_{p} \approx \frac{1}{2 \pi} \frac{K^{2}}{\sigma_{o}^{2}} \quad \text { (plane stress) }
$$

where

$$
r_{p} \approx \frac{1}{6 \pi} \frac{K^{2}}{\sigma_{o}^{2}} \quad \text { (plane strain) }
$$

$r_{p}$ for plane strain is smaller than plane stress, which is because the triaxial stress field suppresses the plastic deformation

$$
K_{e f f}=\sigma \sqrt{\pi a^{\prime}}
$$

$K_{\text {eff }}=$ effective stress intensity factor

Irwin's correction to the fracture toughness of a center-notched tensile specimen

$$
K=\sigma \sqrt{\pi a^{\prime}}\left[\frac{w}{\pi a^{\prime}} \tan \frac{\pi a^{\prime}}{w}+\frac{1}{2 w} \frac{K^{2}}{\sigma_{o}^{2}}\right]
$$



Onset of plastic deformation at the crack-tip

## Plane stress vs plane strain



## Example

- A steel plate with a through thickness crack of length $2 \mathrm{a}=20 \mathrm{~mm}$ is subjected to a stress of 400 Mpa normal to the crack. If the yield strength of the steel is 1500 Mpa , what is the plastic zone size and the stress intensity factor for the crack. Assume that the plate is infinitely wide.


## Dugdale plastic strip model

Dugdale has proposed the crack tip plastic zone model for plane stress case.

Dugdale considered the plastic regions to take a form of narrow strips extending a length R .

Assuming there is an elastic crack of length $2(c+R)$ and the region of length $R$ is closed up by applying compressive stresses normal to the surface. Dugdale demonstrated that

$$
c / a=\cos \left(\frac{\pi}{2} \frac{\sigma}{\sigma_{o}}\right)
$$

Where $a=\mathrm{c}+\mathrm{R}$

$$
R / c=\sec \left(\frac{\pi}{2} \frac{\sigma}{\sigma_{o}}\right)-1
$$

When the applied stresses $\sigma \ll \sigma_{o}, \quad R=\frac{\pi^{2} \sigma^{2} c}{8 \sigma_{o}^{2}}=\frac{\pi K^{2}}{8 \sigma_{o}^{2}}$

